



MATFLOW

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Page : i

Title

MATFLOW V3.2 MODULE APPLICATION MANUAL

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MATFLOW

Ref : M&S.NT.CT.4632.99
Issue : 01 Rev. : 00
Date : 13/04/2004
Page : ii

SUMMARY

This document is the application manual of the MATFLOW 3.2 module.

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MATFLOW

Ref : M&S.NT.CT.4632.99
Issue : 01 Rev. : 00
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Page : iii

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MATFLOW

Ref : M&S.NT.CT.4632.99
Issue : 01 Rev. : 00
Date : 13/04/2004
Page : iv

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Page	Issue/ Rev.	Page	Issue/ Rev.	Page	Issue/ Rev.	Page	Issue/ Rev.	Page	Issue/ Rev.	Page	Issue/ Rev.
All	00/00										
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MATFLOW

Ref : M&S.NT.CT.4632.99
Issue : 01 Rev. : 00
Date : 13/04/2004
Page : 1

MATFLOW V3.2 – Application Manual

This Manual contains task-oriented instructions that show you how to use the MATFLOW module.

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MATFLOW

Ref : M&S.NT.CT.4632.99
Issue : 01 Rev. : 00
Date : 13/04/2004
Page : 2

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TABLE OF CONTENTS

1	REFERENCE DOCUMENTS	4
2	INTRODUCTION.....	5
1.1	FUNCTIONAL DESCRIPTION	5
1.2	METHOD OF ANALYSIS.....	5
1.3	SOFTWARE LIMITATIONS.....	6
2	MATFLOW INPUT/OUTPUT	7
2.1	MATFLOW ARCHITECTURE.....	7
2.2	MATFLOW INPUT FILES DESCRIPTION.....	8
2.2.1	.THERMO file.....	8
2.2.2	.T45 file.....	8
2.2.3	.MFI file.....	8
2.3	MATFLOW OUPUT FILES DESCRIPTION	13
2.3.1	.FLOW file.....	13
2.3.2	.T47 file.....	13
2.3.3	.T48 file.....	13
2.3.4	.MFO file	13

1 REFERENCE DOCUMENTS

- [RD1] "PLUME V3.2" – Interface files definition. P. Chèoux-Damas. Doc. MMS : S413/RT/41.97.
24/10/97
- [RD2] "PLUMFLOW V3.2 procedure – Application manual". C. Theroude. Doc. Astrium :
MOS.NT.CT.3682776.02, Issue : 01, 14/04/2004.

2 INTRODUCTION

1.1 FUNCTIONAL DESCRIPTION

The MATFLOW computer program is used to extend the expansion of the gas/particles plume from the TPPLUME or NAVIER computation domain to the 'infinity'.

The objective of the MATFLOW module is :

according to :

- the results of TPPLUME or NAVIER computation
- the dimensions of the region to be computed

compute :

- the gas streamlines and to extend them to the free molecular far-field in a manner suitable for the future plume impingement predictions by MATPLIMP.
- the particle streamlines, for the prediction of radiative heat fluxes by PLUMRAD.
- the interface files to the graphical module TRAJET for flow-field visualisations.

1.2 METHOD OF ANALYSIS

- streamlines computation : The streamlines determination is performed by linear interpolation from the points of the L.R.C. net. They are built point after point, being considered as iso-mass-flow-rate lines. Each point of a streamline has the same stream function (the stream function is computed by TPPLUME or NAVIER).
- source-flow method : The streamlines, computed by the M.O.C., are extended in the far flow-field by the source-flow method up to the SMAX distance, defined by the user, as following :
 1. first, the streamlines are extended, by straight lines passing through the source-points. Two source-points are considered :
 - one in the centre of the nozzle exit plan (on the axis) which allows to know the flow up to an angle of $\pi/2$ between the velocity direction and the axis.
 - another, at the nozzle lip, is used to describe the back-flow.
 2. values of the area ratio along streamlines are then computed (those values are function only of the geometrical pattern of streamlines). Following, flow-field properties such ρ , T , V are computed, using the previously computed area ratio, and assuming isentropic expansion.
 3. to improve the regularity of the streamlines mesh, the points are then re-distributed on each streamline according to a geometrical progression law. The flow parameters are computed at new point by interpolation between two old points.

1.3 SOFTWARE LIMITATIONS

The area of the M.O.C. domain must be large enough to fit with the hypothesis of a source-flow at the boundary.

At the end of a MATFLOW execution, it is recommended to run 'TRAJET' in order to check that the results are consistent.

2 MATFLOW INPUT/OUTPUT

2.1 MATFLOW ARCHITECTURE

The MATFLOW input files are :

File	Function
"thruster name".THERMO	Gas table giving versus the temperature : H, W_{mol} , γ , T, P, C_p , μ , Pr.
"thruster name".T45	Flow-field file of characteristic line data giving the temperature , the density, the velocity of the gas and possibly of the particles.
"thruster name".MFI	User input file.

The MATFLOW output files are :

File	Function
"thruster name".FLOW	Flow-field parameters and nozzle geometry.
"thruster name".T47	Coordinates of the points along the L.R.C..
"thruster name".T48	Particle flow-field data along streamlines.
"thruster name".MFO	Output listing file.

All these files are displayed on Figure 2.2-1.

2.2 MATFLOW INPUT FILES DESCRIPTION

2.2.1 .THERMO file

This is the interface file from ODE. Gas table giving, versus the temperature : H , W_{mol} , γ , T , P , C_p , μ , Pr .

2.2.2 .T45 file

This is the interface file from NAVIER or TPPLUME. Flow-field file giving the temperature, the density and the velocity of the gas and possibly particles, along characteristic lines.

2.2.3 .MFI file

This is the user input file of MATFLOW. As shown on Figure 2.2-2 for a bipropellant test thruster, it is composed of one namelist called SLIN.

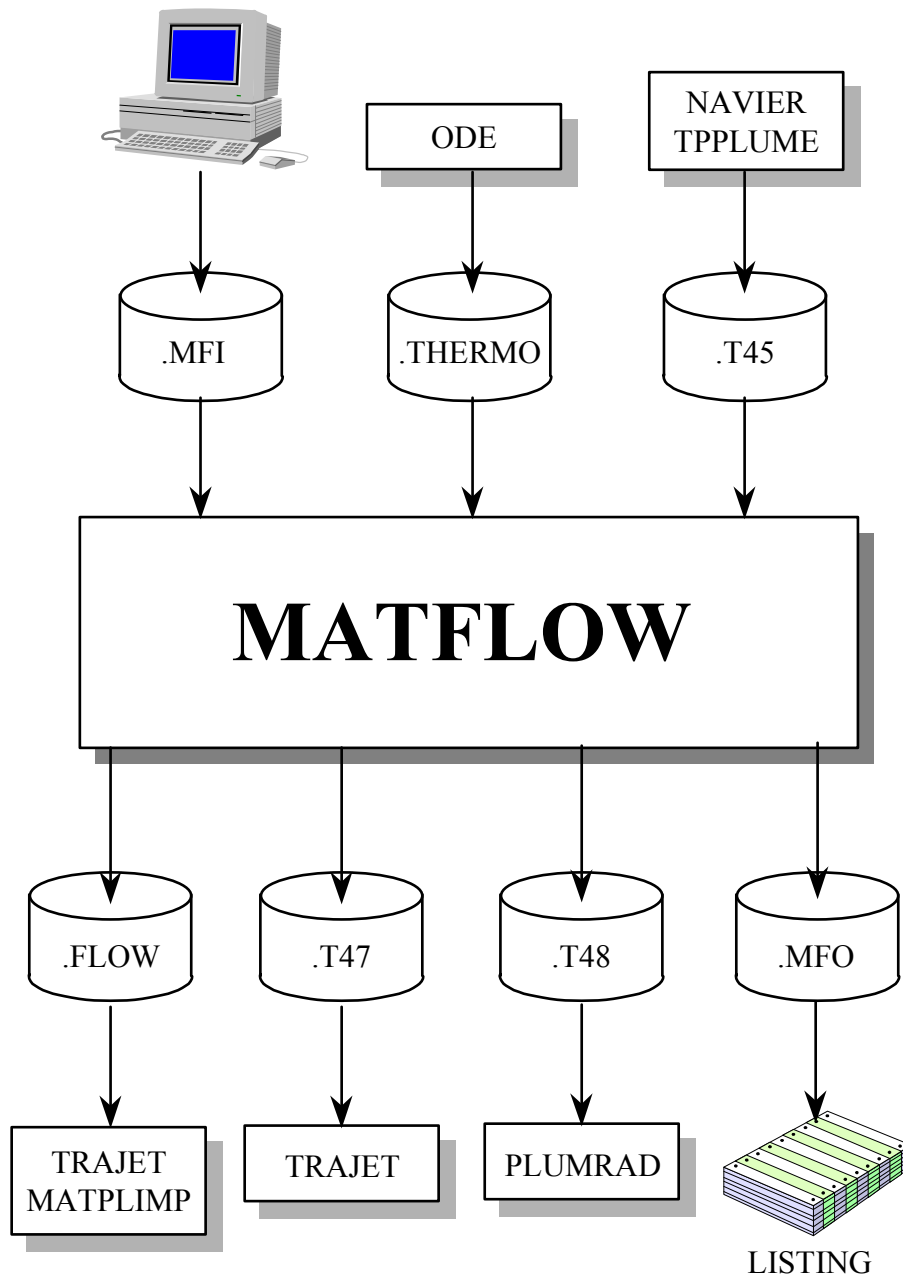


Figure 2.2-1 : MATFLOW architecture.

2.2.3.1 namelist \$SLIN

Purpose :

Input data for MATFLOW.

Format of the file :

```
$SLIN  
  
[NSL=nsl]           [NSP=nsp]           PSI=psi  
[PLIM=plim]        [MRAD=mrad]        [TCHA=tcha]  
[LISSE=lisse]      [PRINTF=printf]    [PRINTG=printg]  
[PRINTP=printp]    [DSMIN=dsmin]      [SMAX=smax]  
  
$END
```

Description :

NSL Number of gas streamlines.

Type : integer
Range : $2 \leq nsl \leq 40$
Default : 25

NSP Number of particles streamlines.

Type : integer
Range : $2 \leq nsl \leq 40$
Default : 15

PSI Gas stream function for each streamline, no dimension.

Type : real
Range : $0 \leq psi \leq 1$
Default : linear distribution by MATFLOW

Note : nsl values are given, up to 40 values can be specified, separated by commas

PLIM	specifies whether the interface file with MATPLIMP is created. Range : T, F Default : T
MRAD	specifies whether the interface file with PLUMRAD is created. Range : T, F Default : F
TCHA	specifies whether the characteristic lines file (.T47) for TRAJET is created. Range : T, F Default : F
LISSE	specifies whether the values are to be smoothed on the streamlines. Range : T, F Default : T
PRINTF	specifies whether the data from TPPLUME or NAVIER are to be printed. Range : T, F Default : F
PRINTG	specifies whether the result from the gas streamlines computation have to be printed. Range : T, F Default : F
PRINTP	specifies whether the result from the particles streamlines computation have to be printed. Range : T, F Default : F Note : only to be specified if MRAD=TRUE.

DSMIN specifies the minimal distance, between two points of a streamline to keep the second point, adim (*).

Type : real

Range : > 0

Default : 0.02

SMAX specifies the distance to the exit section up to which the flow is to be extended by the source-point method, adim (*).

Type : real

Range : > 0

Default : 2000

Remarks :

The "adim (*)" note means the parameters are normalised by the throat radius RSTAR (see namelist \$GEONZO).

```
$SLIN
NSL = 23 ,
PSI = .00 , .01 , .04 , .100 , .200 , .300 , .400 , .500 , .600 , .700 ,
      .80 , .88 , .93 , .96 , .98 , .99 , .996 , .998 , .999 , .9997 ,
      .99989 , .99995 , .99999
PLIM = T , SMAX = 20000. , DSMIN = 0.1 ,
LISSE = T , TCHA=F , PRINTG=F,
$END
```

Figure 2.2-2 : test.MFI : example of input file for MATFLOW.

2.3 MATFLOW OUTPUT FILES DESCRIPTION

2.3.1 .FLOW file

This is an interface file to TRAJET and MATPLIMP, it contains the nozzle and flow parameters arranged by streamlines.

2.3.2 .T47 file

This is an interface file to TRAJET, it contains the coordinates of the points along the L.R.C..

Note : this file is created only if the user has specified it in the MATFLOW input file.

2.3.3 .T48 file

This is the interface file to PLUMRAD, it contains the particle flow description along the streamlines.

2.3.4 .MFO file

This is the listing file of MATFLOW.

The output listing file is composed of six parts, described on Figure 2.3-1 to Figure 2.3-5, depending on the values of the printing parameters : PRINTF, PRINTG, PRINTP and a review of the input file "thruster name".MFI.(see Figure 2.3-1) :

1. Printing of the namelist \$SLIN. The meaning of the parameters is given in the input file description.
2. summary of ODE results (conditions in the chamber) and nozzle geometry (see Figure 2.3-2).
3. printing of the file "thruster name".T45, if PRINTF = F (see Figure 2.3-3).

LRC : number of the current L.R.C..

MS : parameter defining the L.R.C. :

MS = -1 : the L.R.C. comes from the transonic region,

MS = 0 : the L.R.C. is the start line,

MS = 1 : the current L.R.C. is inside the nozzle,

MS = 2 : the L.R.C. is in the free plume.

JP : number of points on the L.R.C..

J : index of the point on the L.R.C..

Z/R*, R/R* : axial and radial coordinate normalized by the throat radius.

ID : point identification :

ID = 2 : current point,

ID = 3 : axis point,

ID = 5 : wall point.

P : gas pressure.

RHO : gas density.

ANGLE : angle between the gas velocity and the axis.

V : radial coordinate of the gas velocity.

PSI : stream function.

4. computed mass flow rates and thrust (see Figure 2.3-4).

The thrust value computed in MATFLOW is different from that computed in TPPLUME and NAVIER. When using MATFLOW, the integration is done on the first L.R.C., taking into account the boundary layer effect and the Prandtl-Meyer fan at the nozzle lip while TPPLUME computes with the last L.R.C. of the replaced nozzle contour.

The table MASS FLOW RATE CONSERVATION shows the importance of the flow rate loss, integrated at a given point of the streamlines meshing, due to the accumulated inaccuracies of the M.O.C. computation and linear interpolations during the streamlines calculation and the remeshing of the points.

The source-flow method insures the rigorous mass flow rate conservation.

5. printing of the gas streamlines, if PRINTG = T (see Figure 2.3-5).

I : number of the point.

Z/R*, R/R* : axial and radial coordinate normalized by the throat radius.

RHO : gas density.

T : gas temperature.

P : gas pressure.

VEL : velocity of the gas flow.

ANGLE : angle between the gas velocity and the axis.

BIRD : Bird parameter (for the transitional regime).

6. printing of the particle streamlines, if PRINTP = T.

The particles streamlines are arranged by group, corresponding to a given diameter.

These parameters are described below :

I : number of the current point.

Z/Z*, R/R* : axial and radial coordinates normalized by the throat radius.

T : temperature of the particles.

RHO : density of the particles set.

V : velocity of the particles.

The following example of listing is coming from the bipropellant test thruster computation.

```
-----
--          TITLE OF ODE INPUT FILE :   Bi-propellant test thruster for PLUMFLOW demonstration          DATE : 14-Apr-
2004
-----
                                     NAMEDLIST SLIN
-----

NUMBER OF GAS STREAMLINES          NSL =   23
NUMBER OF PARTICLE STREAMLINES     NSP =   15
GAS STREAM FUNCTION                 PSI =   0.0000  0.0100  0.0400  0.1000  0.2000  0.3000
                                     0.4000  0.5000  0.6000  0.7000  0.8000  0.8800
                                     0.9300  0.9600  0.9800  0.9900  0.9960  0.9980
                                     0.9990  0.9997  0.9999  0.9999  1.0000

FLOW COMPUTATION FOR MATPLIMP        PLIM =  TRUE
NO INTERFACE FILE WITH PLUMRAD       MRAD = FALSE
LRC ARE NOT STORED                   TCHA = FALSE
THE STREAMLINE VALUES ARE POLISHED  LISSE =  TRUE
THE DATA FROM TPPLUME ARE PRINTED   PRINTF = TRUE
THE GAS STREAMLINES ARE PRINTED      PRINTG = TRUE
THE PARTICLE STREAMLINES ARE NOT PRINTED PRINTP = FALSE
MINIMAL DISTANCE BETWEEN 2 POINTS OF A STREAMLINE  DSMIN =  0.1000
FLOW FIELD EXTENSION LENGTH          SMAX = 20000.00
```

Figure 2.3-1 : test.MFO : echo of the user input file : namelist \$SLIN

```
-----
--          TITLE OF ODE INPUT FILE :   Bi-propellant test thruster for PLUMFLOW demonstration          DATE : 14-Apr-
2004
-----

FLOW PARAMETERS ARE COMPUTED BY NAVIER

IDEAL GAS : CP AND GAMMA ARE CONSTANT

CONDITION IN THE CHAMBER :
-----

PRESSURE          PC =   6.38000 (BAR)
TEMPERATURE       TC =  1120.00000 (DEG K)
DENSITY           RHOG0 =  0.73309 (KG/M3)
GAS CONSTANT      RGAS =  777.04767 (J/KG/DEG K)
SPECIFIC HEAT RATIO GAMMA =  1.35700
GAS SPECIFIC HEAT CPGAS = 2953.65186 (J/KG/DEG K)

NOZZLE GEOMETRY :
-----

THROAT RADIUS     RSTAR =  0.00079 (M)
EXIT RADIUS       REXIT =  0.00563 (M)
DISTANCE THROAT-EXIT =  0.01212 (M)
```

Figure 2.3-2 : test.MFO : summary of the chamber conditions and nozzle geometry

```

-----
--                               TITLE OF ODE INPUT FILE :      Bi-propellant test thruster for PLUMFLOW demonstration      DATE : 14-Apr-
2004
-----
LRC = 25    MS = 0    JP = 49
J      Z/R*    R/R*    ID      T(K)      RHO(KG/M3)  ANGLE      V(M/S)    PSI
1      0.0000  0.0000  1      977.154   0.4974E+00  0.0000E+00  0.9210E+03 0.0000000
2      0.0000  0.0722  1      976.919   0.4969E+00  -0.2386E+00  0.9219E+03 0.005480
3      0.0000  0.1393  1      976.299   0.4958E+00  -0.4601E+00  0.9239E+03 0.020396
4      0.0000  0.2017  1      975.301   0.4942E+00  -0.6532E+00  0.9270E+03 0.042740
5      0.0000  0.2596  1      974.018   0.4920E+00  -0.8233E+00  0.9312E+03 0.070832
6      0.0000  0.3135  1      972.502   0.4895E+00  -0.9671E+00  0.9361E+03 0.103267
7      0.0000  0.3635  1      970.808   0.4867E+00  -0.1088E+01  0.9416E+03 0.138875
8      0.0000  0.4101  1      968.980   0.4836E+00  -0.1186E+01  0.9475E+03 0.176682
9      0.0000  0.4533  1      967.050   0.4803E+00  -0.1262E+01  0.9538E+03 0.215883
10     0.0000  0.4934  1      965.056   0.4769E+00  -0.1319E+01  0.9603E+03 0.255815
11     0.0000  0.5308  1      963.033   0.4733E+00  -0.1357E+01  0.9669E+03 0.295939
12     0.0000  0.5654  1      960.996   0.4696E+00  -0.1378E+01  0.9736E+03 0.335816
13     0.0000  0.5977  1      958.986   0.4659E+00  -0.1383E+01  0.9804E+03 0.375095
14     0.0000  0.6276  1      957.008   0.4621E+00  -0.1375E+01  0.9871E+03 0.413499
15     0.0000  0.6554  1      955.096   0.4582E+00  -0.1354E+01  0.9937E+03 0.450812
16     0.0000  0.6813  1      953.256   0.4544E+00  -0.1322E+01  0.1000E+04 0.486872
17     0.0000  0.7053  1      951.512   0.4505E+00  -0.1280E+01  0.1006E+04 0.521561
18     0.0000  0.7277  1      949.861   0.4466E+00  -0.1229E+01  0.1013E+04 0.554794
19     0.0000  0.7484  1      948.323   0.4428E+00  -0.1171E+01  0.1018E+04 0.586522
20     0.0000  0.7677  1      946.899   0.4390E+00  -0.1107E+01  0.1024E+04 0.616715
21     0.0000  0.7856  1      945.591   0.4352E+00  -0.1037E+01  0.1029E+04 0.645368
22     0.0000  0.8023  1      944.388   0.4315E+00  -0.9640E+00  0.1034E+04 0.672492
23     0.0000  0.8178  1      943.288   0.4278E+00  -0.8879E+00  0.1039E+04 0.698112
24     0.0000  0.8322  1      942.281   0.4243E+00  -0.8087E+00  0.1044E+04 0.722267
25     0.0000  0.8455  1      941.369   0.4207E+00  -0.7281E+00  0.1049E+04 0.745008
26     0.0000  0.8589  1      940.445   0.4171E+00  -0.6394E+00  0.1054E+04 0.768017
27     0.0000  0.8713  1      939.629   0.4135E+00  -0.5477E+00  0.1057E+04 0.789586
28     0.0000  0.8828  1      938.933   0.4100E+00  -0.4565E+00  0.1061E+04 0.809770
29     0.0000  0.8935  1      938.317   0.4066E+00  -0.3658E+00  0.1063E+04 0.828625
30     0.0000  0.9034  1      937.783   0.4033E+00  -0.2769E+00  0.1065E+04 0.846213
  
```

Figure 2.3-3 : test.MFO : printing of the file "thruster name".T45

```

-----
--                               TITLE OF ODE INPUT FILE :      Bi-propellant test thruster for PLUMFLOW demonstration      DATE : 14-Apr-
2004
-----
                        COMPUTED MASS FLOW RATES AND THRUST
                        -----

MASS FLOW RATE =  0.9047E-03 KG/S      THRUST =  0.2093E+01 N

MASS FLOW RATE CONSERVATION:

    1.0000    1.0023    1.0044    1.0056    1.0065
    1.0068    1.0075    1.0088    1.0111    1.0112
    1.0110    1.0100    1.0098    1.0119    1.0097
    1.0115    1.0054    1.0066    1.0105    1.0212
    1.0375    1.0554    1.0582    1.0505    1.0476
    1.0539    1.0608    1.0581    1.0550    1.0542
    1.0561    1.0561    1.0561    1.0561    1.0562
    1.0562    1.0562    1.0562    1.0562    1.0563
    1.0563    1.0563    1.0563    1.0563    1.0563
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564    1.0564    1.0564    1.0564
    1.0564    1.0564

MASS FLOW RATIO PER STREAMLINE
                        -----

                            0.9592    0.9777
                            1.0265    1.0508
                            1.0617    1.0936
                            1.0992    1.0974
                            1.0642    1.0947
                            1.0388    0.9894
                            0.9902    0.9740
                            0.9507    0.8892
                            1.2750    0.9559
                            0.9977    0.9897
                            1.0317    1.1207
  
```

Figure 2.3-4 : test.MFO : mass flow rate conservation



MATFLOW

Ref : M&S.NT.CT.4632.99
 Issue : 01 Rev. : 00
 Date : 13/04/2004
 Page : 18

 TITLE OF ODE INPUT FILE : Bi-propellant test thruster for PLUMFLOW demonstration DATE : 14-Apr-2004

LINE NO 1 MASS FRACTION : 0.000000 NUMBER OF POINTS OF THE M.O.C. : 65

I	Z/R*	R/R*	RHO (KG/M3)	T (DEG K)	P (PA)	VEL (M/S)	ANGLE (DEG)	BIRD
1	15.9	0.0	.136E-02	120.50	.127E+03	2430.63	0.00	0.00
2	16.4	0.0	.128E-02	118.01	.117E+03	2433.71	0.00	0.00
3	16.9	0.0	.120E-02	115.43	.107E+03	2436.84	0.00	0.00
4	17.5	0.0	.111E-02	112.79	.977E+02	2440.05	0.00	0.00
5	18.1	0.0	.103E-02	110.04	.884E+02	2443.39	0.00	0.00
6	18.8	0.0	.955E-03	107.06	.795E+02	2446.84	0.00	0.00
7	19.5	0.0	.881E-03	104.07	.712E+02	2450.38	0.00	0.01
8	20.3	0.0	.809E-03	101.06	.636E+02	2453.99	0.00	0.01
9	21.2	0.0	.742E-03	98.03	.565E+02	2457.64	0.00	0.01
10	22.2	0.0	.678E-03	94.95	.500E+02	2461.30	0.00	0.01
11	23.3	0.0	.618E-03	91.82	.441E+02	2464.91	0.00	0.01
12	24.5	0.0	.562E-03	88.73	.388E+02	2468.41	0.00	0.01
13	25.8	0.0	.511E-03	85.87	.341E+02	2471.73	0.00	0.01
14	27.2	0.0	.469E-03	83.38	.304E+02	2474.84	0.00	0.01
15	28.8	0.0	.427E-03	81.07	.269E+02	2477.57	0.00	0.01
16	30.6	0.0	.389E-03	77.86	.235E+02	2479.22	0.00	0.00
17	32.5	0.0	.375E-03	78.06	.228E+02	2477.83	0.00	0.00
18	34.6	0.0	.341E-03	75.71	.201E+02	2468.78	0.00	0.00
19	37.0	0.0	.373E-03	62.54	.181E+02	2445.80	0.00	0.02
20	39.5	0.0	.913E-03	114.33	.811E+02	2408.63	0.00	0.02
21	42.3	0.0	.259E-02	184.88	.372E+03	2368.85	0.00	0.00
22	45.4	0.0	.433E-02	218.72	.737E+03	2341.46	0.00	0.00
23	48.8	0.0	.431E-02	219.21	.734E+03	2333.95	0.00	0.00
24	52.6	0.0	.315E-02	198.00	.484E+03	2344.00	0.00	0.00
25	56.7	0.0	.215E-02	170.64	.285E+03	2363.94	0.00	0.00
26	61.3	0.0	.150E-02	149.17	.174E+03	2386.45	0.00	0.00
27	66.3	0.0	.106E-02	131.77	.108E+03	2407.30	0.00	0.00
28	71.8	0.0	.790E-03	118.53	.728E+02	2425.19	0.00	0.00
29	77.8	0.0	.602E-03	107.48	.503E+02	2440.36	0.00	0.00
30	84.4	0.0	.452E-03	96.83	.340E+02	2453.28	0.00	0.00
31	91.8	0.0	.342E-03	87.35	.232E+02	2464.17	0.00	0.00
32	99.8	0.0	.264E-03	79.81	.164E+02	2472.90	0.00	0.00
33	108.6	0.0	.206E-03	73.15	.117E+02	2479.22	0.00	0.00
34	118.4	0.0	.166E-03	67.54	.873E+01	2485.72	0.00	0.00
35	129.1	0.0	.135E-03	62.57	.658E+01	2491.47	0.00	0.01
36	140.9	0.0	.111E-03	58.07	.499E+01	2496.66	0.00	0.01
37	153.8	0.0	.906E-04	53.94	.380E+01	2501.41	0.00	0.01
38	168.1	0.0	.743E-04	50.13	.290E+01	2505.79	0.00	0.01
39	183.7	0.0	.610E-04	46.60	.221E+01	2509.83	0.00	0.01
40	201.0	0.0	.502E-04	43.33	.169E+01	2513.58	0.00	0.01
41	219.9	0.0	.412E-04	40.30	.129E+01	2517.04	0.00	0.01
42	240.8	0.0	.339E-04	37.48	.988E+00	2520.26	0.00	0.01
43	263.7	0.0	.279E-04	34.87	.756E+00	2523.23	0.00	0.01
44	289.0	0.0	.230E-04	32.45	.579E+00	2526.00	0.00	0.01
45	316.7	0.0	.189E-04	30.19	.444E+00	2528.56	0.00	0.01
46	347.3	0.0	.156E-04	28.10	.340E+00	2530.94	0.00	0.01
47	380.9	0.0	.128E-04	26.16	.261E+00	2533.15	0.00	0.01
48	417.8	0.0	.106E-04	24.35	.200E+00	2535.20	0.00	0.01
49	458.5	0.0	.872E-05	22.67	.154E+00	2537.11	0.00	0.02
50	503.2	0.0	.719E-05	21.10	.118E+00	2538.88	0.00	0.02
51	552.4	0.0	.593E-05	19.65	.905E-01	2540.52	0.00	0.02

Figure 2.3-5 : test.MFO : printing of the gas streamlines

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